

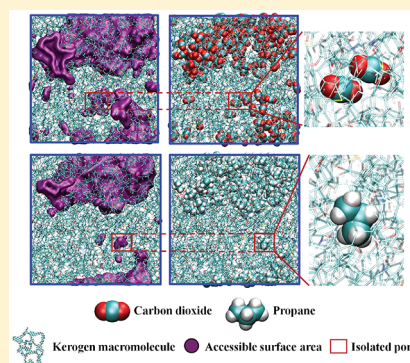
# Deformation and Swelling of Kerogen Matrix in Light Hydrocarbons and Carbon Dioxide

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## S Supporting Information

**ABSTRACT:** Shale gas has become an attractive alternative to conventional fossil fuels due to its clean-burning characteristics. Fluid molecules reside in micropores and mesopores in shale formations. Molecular simulations provide insights into the kerogen structures, adsorption of hydrocarbons and carbon dioxide, and kerogen swelling. In this work, a new approach is introduced to create atomistic configurations of kerogen matrix with specific porosity. A dummy particle is used to control the porosity. Once the kerogen matrix is created, the dummy particle is removed and a limited number of nails are placed on the periphery of the pores to prevent the kerogen matrix from collapsing and to keep its basic structure intact. The hybrid Molecular Dynamics-Grand Canonical Monte Carlo (MD-GCMC) simulations are performed to investigate the adsorption and kerogen swelling of five hydrocarbon gases (methane, ethane, propane, *n*-butane, and *i*-butane at 393.15 K and various pressures), *n*-pentane liquid (at 298.15 K and 1 atm), and supercritical carbon dioxide (at 393.15 K to a pressure of 400 atm). The kerogen matrix is flexible.

Our simulation results show that there is a coupling between adsorbate molecular size and shape and deformation of the kerogen matrix structure. The flexibility of the kerogen matrix affects swelling. The kerogen matrix deformation allows small adsorbate molecules to dissolve in the matrix. Our simulations results show that kerogen swelling decreases with the increase of the molecular size of the adsorbate ( $\text{CO}_2 > \text{CH}_4 > \text{C}_2\text{H}_6 > \text{C}_3\text{H}_8$ ). The deformation and increase in swelling by *n*-pentane is much more pronounced than by methane and other light hydrocarbon gases. Our work is based on type II-A kerogen macromolecules. The methodology can be applied to other types of kerogen molecules.



## INTRODUCTION

Shale gas has changed the energy landscape of the conventional fossil fuels. Natural gas is a clean-burning fuel and produces less  $\text{CO}_2$  compared to crude oil. The United States (U.S.) has become the major shale gas producer in the world. In 2017, the total production of dry natural gas was about 17 trillion cubic feet (Tcf) per year from shale resources in the U.S. This corresponds to 62% of total U.S. dry natural gas production in that year.<sup>1</sup> Despite the high production of hydrocarbons from shale oil/gas reservoirs, the recovery factor is very low. A better understanding of the shale physicochemical properties may lead to new processes to improve shale gas recovery as well as advancing the environmental stewardship.

Shale rock is composed of inorganic minerals and organic matter. The organic matter is mainly composed of kerogens. Kerogen is insoluble in common polar solvents;<sup>2</sup> it is essentially composed of polydisperse macromolecules. Shale gas resides in micropores and mesopores.<sup>3,4</sup> The fluids in the kerogen matrix can be in three different states: (i) adsorbed state on the kerogen surface, (ii) free molecules in the pores, and (iii) dissolved molecules in the kerogen matrix.<sup>5</sup> The physicochemical properties of kerogen depend on its origin

and on its burial history.<sup>6,7</sup> Different kerogen types<sup>8–10</sup> can be distinguished: (i) type I from a lacustrine anoxic environment, (ii) type II from marine shale and continental planktons, (iii) type III from plants in tertiary and quaternary coals, and (iv) type IV from older sediments redeposited after erosion. In the geological medium, kerogen is exposed to constraints such as temperature and pressure. Under these conditions the type of kerogen affects the microstructure and on the fluid behavior confined in kerogen pores. The interplay between gas adsorption, structural deformation, and the swelling and shrinkage of the kerogen may relate to increase in shale gas production. This interplay is not well understood. The adsorption and swelling of kerogen media by gases ( $\text{CH}_4$ ,  $\text{C}_2\text{H}_6$ ,  $\text{C}_3\text{H}_8$ , *n*- $\text{C}_4\text{H}_{10}$ , *i*- $\text{C}_4\text{H}_{10}$  and  $\text{CO}_2$ ) and liquid *n*- $\text{C}_5\text{H}_{12}$  is the focus of this work.

Adsorption is strongly linked to the accessible surface area and the porosity. Experimental research has mostly focused on adsorption in shale samples.<sup>11–22</sup> Recent studies investigate the

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adsorption of light hydrocarbon gases ( $\text{CH}_4$ ,  $\text{C}_2\text{H}_6$ ,  $\text{C}_3\text{H}_8$ ,  $n\text{-C}_4\text{H}_{10}$  and  $i\text{-C}_4\text{H}_{10}$ ) and carbon dioxide in isolated kerogen.<sup>17,23–27</sup> Kerogen pore structure may deform from gas adsorption. The fluids may dissolve in the kerogen, adding to swelling. Extensive experimental studies on kerogen swelling in several liquid hydrocarbons have been reported at room temperature and atmospheric pressure.<sup>28–36</sup> The measurements reveal that (i) the swelling decreases as the maturity of the rock increases, (ii) the effect of temperature is not as pronounced as maturity, and (iii) samples prepared by pretreatment temperature swell differently compared to nontreated samples. Larsen and Li<sup>28,30</sup> (kerogen type I and II), Larsen et al.<sup>31</sup> (different kerogen types II) and Ballice et al.<sup>32</sup> (kerogen type I and II) use the volumetric swelling method to measure the swelling of kerogen by  $n\text{-C}_5\text{H}_{12}$  at room temperature and atmospheric pressure. They find the kerogen samples swell from 15 to 24%. The measurements at high pressure are a challenge.

Molecular simulations have also been used to predict swelling. Many computational investigations have been performed to provide insights into kerogen structural properties,<sup>7,37–54</sup> kerogen adsorption properties,<sup>7,39,46–50,52,53,55–62</sup> but swelling of kerogen has been studied in a limited number of studies.<sup>7,43,44,49,53</sup>

Three different methods have been used to create kerogen matrix. In one method, the kerogen macromolecules are placed in a box without other species.<sup>7,46–48,50</sup> In another method, the kerogen macromolecules are placed in a box with specific molecules.<sup>39,42,45,54,55,63,64</sup> In a third method, a hybrid reverse Monte Carlo reconstruction technique is used.<sup>37,38,40,51</sup> MD simulations are used for the creation of the initial kerogen structure in the studies mentioned below. Sui and Yao<sup>7</sup> create the kerogen matrix using 6 kerogen macromolecules of type II-A at  $T = 300$  K and  $P = 10$  atm. They calculate methane accessible surface area of  $1548 \text{ m}^2 \text{ g}^{-1}$  and pore volume of  $0.181 \text{ cm}^3 \text{ g}^{-1}$ . They also estimate carbon dioxide accessible surface area of  $1845 \text{ m}^2 \text{ g}^{-1}$  and pore volume of  $0.209 \text{ cm}^3 \text{ g}^{-1}$ . Pathak et al.<sup>43</sup> and Pathak et al.<sup>44</sup> create the kerogen matrix, respectively, using 35 and 15 kerogen macromolecules of type II-C at  $T = 300$  K and  $P = 300$  atm. Pathak et al.<sup>43</sup> do not report the porosity and the accessible surface area. Pathak et al.<sup>44</sup> use a Monte Carlo integration method to report porosity<sup>65</sup> of 3.7%. Wang et al.<sup>53</sup> create the kerogen matrix using 10 kerogen macromolecules of type I-A at  $T = 300$  K and  $P = 197$  atm. Ho et al.<sup>49</sup> create the kerogen matrix using 27 kerogen macromolecules of type II-D at  $T = 300$  K and  $P = 1$  atm. They calculate a porosity close to 26% (based on helium probe particles) and an increase of the accessible surface area (from  $\sim 3\%$  at 1 atm to  $\sim 8\%$  at 192 atm for methane and from  $\sim 6\%$  at 1 atm to  $\sim 18\%$  at 192 atm for  $\text{CO}_2$ ). However, other authors<sup>39,44,45,55,62,66</sup> report a lower porosity, pore volume, and accessible surface area. Collell et al.,<sup>55</sup> Michalec and Lisal,<sup>39</sup> Kazemi et al.<sup>66</sup> and Vasileiadis et al.<sup>45</sup> report a porosity ranging from 0.7 to 2% and an accessible surface area ranging from 4.7 to  $232 \text{ m}^2 \text{ g}^{-1}$ . Trewin et al.<sup>67</sup> point out that a scaling factor should be applied to the calculated accessible surface area and pore volume from the Connolly method to obtain true values. They show that the Connolly method overestimates the accessible surface area and the pore volume. One of the objectives of this investigation is the creation of flexible kerogen matrix to investigate the adsorption of hydrocarbon gases from methane to  $n$ -butane and  $\text{CO}_2$ . In particular, we are interested to examine the 50% difference in adsorption of  $n$ -

butane and  $i$ -butane measured by Zhao et al.<sup>24,25</sup> and Wu et al.<sup>26</sup>

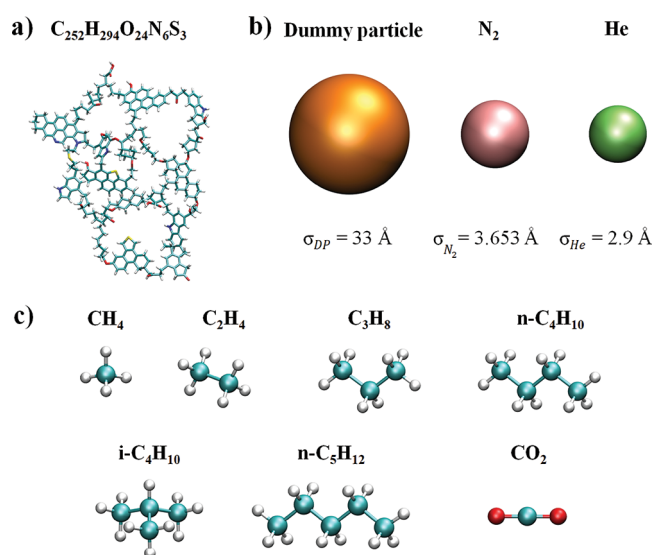
Swelling of kerogen matrix has been investigated by three different methods: (i) the poromechanical model<sup>68,69</sup> (using fixed kerogen volume), (ii) the molecular dynamics simulations, and (iii) the hybrid molecular dynamics-grand canonical Monte Carlo (MD-GCMC) method. Sui and Yao<sup>7</sup> and Wang et al.<sup>53</sup> apply the poromechanical method. They use GCMC simulations to calculate methane and carbon dioxide adsorption isotherms at  $T = 298, 340,$  and  $380$  K and  $P$  to 296 atm (Sui and Yao<sup>7</sup>) and  $T = 298, 328, 358,$  and  $388$  K and  $P = 296$  atm (Wang et al.<sup>53</sup>). Sui and Yao<sup>7</sup> observe that the volumetric strain increases until reaching a plateau. They find that the maximum swellings of kerogen by methane and carbon dioxide are, respectively, 4.45% and 6.52% at 340 K and 148 atm. Wang et al.<sup>53</sup> observe a different trend. The volumetric strain first increases up to a maximum as pressure increases, and then decreases gradually with further pressure increase. They find that the maximum swelling of kerogen by methane is 1.20% (at 298 K and 158 atm), 0.75% (at 328 K and 128 atm), 0.55% (at 358 K and 128 atm), and 0.3% (at 388 K and 89 atm). Pathak et al.<sup>44</sup> use MD simulations to study the swelling of a type II-C kerogen matrix at 400 K and 300 atm. They investigate four different cases: (i) pure kerogen in order to calculate the volume of the simulation box without adsorbate ( $V_{\text{kerogen w/o adsorbate}}$ ), (ii) 15 kerogen molecules with 750 methane molecules, (iii) 15 kerogen molecules with 750 carbon dioxide molecules, and (iv) 15 kerogen molecules with  $\text{CH}_4$  and  $\text{CO}_2$  molecules (in a 1:3 molecular ratio with a total of 750 molecules). They find that the swelling of kerogen by methane, carbon dioxide and  $\text{CH}_4$  and  $\text{CO}_2$  mixture is, respectively, 74%, 54%, and 54%. Note that in this method swelling may be a function of mixing of the number of molecules. Pathak et al.<sup>43</sup> use the same methodology to investigate the swelling of a type II-C kerogen matrix by different liquids (based on a fixed mass of kerogen and a 20% mass of liquid hydrocarbons) at 300 and 375 K and 1 and 300 atm. They observe that different liquid hydrocarbons swell kerogen differently; the swelling is more pronounced by polar and aromatic hydrocarbons than by other liquids. Ho et al.<sup>49</sup> use the MD-GCMC method to investigate the swelling of a type II-D kerogen matrix by methane, carbon dioxide, and helium at  $T = 300$  K and  $P$  to 192 atm. They report that the volumetric strain increases with increasing pressure and it is less than 0.5%, 5.4% and 11% when calculated by He,  $\text{CH}_4$ , and  $\text{CO}_2$ , respectively, at  $T = 300$  K and  $P = 192$  atm. There are various evidence that adsorption and swelling are affected by flexibility of kerogen matrix.<sup>62,70</sup> One objective of this investigation is further study of adsorption and swelling of kerogen matrix to a pressure of 400 atm. Another objective is the investigation of adsorption of  $n\text{-C}_4\text{H}_{10}$  and  $i\text{-C}_4\text{H}_{10}$  because of the significant difference in adsorption measurements of the two fluids.

We aim to investigate swelling in gases (methane, ethane, propane,  $n$ -butane,  $i$ -butane, and carbon dioxide) and liquid  $n$ -pentane based on molecular simulations of fully flexible macromolecules. A key point of this investigation is to find out the difference in swelling, and pore structure deformation in gases and liquids. The manuscript is organized as follows. After the introduction, the kerogen, hydrocarbons, and  $\text{CO}_2$  molecular models are provided as well as the computational details. Then, the process to create the kerogen matrix is presented. Next, we investigate adsorption of each adsorbate

and the swelling and the kerogen matrix deformation. At the end, we draw conclusions.

## MATERIALS AND METHODS

**Atomistic Models.** Type II-A kerogen macromolecule ( $M_{C_{252}H_{294}O_{24}N_6S_3} = 3887 \text{ g mol}^{-1}$  proposed by Ungerer et al.<sup>2</sup>), dummy particle ( $\sigma_{DP} = 33 \text{ \AA}$ ), probe particles nitrogen ( $\sigma_{N_2} = 3.653 \text{ \AA}$ ), and helium ( $\sigma_{He} = 2.9 \text{ \AA}$ ), various hydrocarbon gases (methane, ethane, propane, *n*-butane, and *i*-butane), liquid *n*-pentane and carbon dioxide are included in this study. The graphical user interface (GUI) of the Medea software environment<sup>71</sup> (version 2.21) is used to create a fully flexible kerogen matrix. The kerogen matrix has a chemical composition close to the isolated kerogen samples used in adsorption measurements in our laboratory.<sup>24–26</sup> All the species are illustrated in Figure 1 and the physicochemical



**Figure 1.** (a) Type II-A kerogen macromolecule. (b) Dummy particle and probe particles He and  $N_2$ . (c) Molecular structure of methane, ethane, propane, *n*-butane, *i*-butane, *n*-pentane, and the carbon dioxide. Color code: cyan (C), white (H), red (O), yellow (S), blue (N), orange (DP), pink ( $N_2$ ) and lime (He). The dummy particle and probe particles are represented by a single sphere.

properties of the type II-A kerogen are listed in Table S1 in the Supporting Information (SI). In this work, one dummy particle is introduced to create large pores and a porosity of around 10%. Probe particles He and  $N_2$  are used to calculate the accessible surface area and porosity, respectively.

**Simulation Methods.** The polymer consistent force field plus (PCFF+) <sup>71–74</sup> is used to model all the molecules. PCFF+ is an all atom force field developed by Materials Design<sup>71</sup> to study the properties of organic matter including polymers and kerogens with high accuracy. It is a second generation force field belonging to the family of the consistent force field (such as the condensed-phase optimized molecular potentials for atomistic simulation studies force field<sup>75–79</sup> (COMPASS)). The total potential consists of seven terms:

$$V_{\text{total}} = V_{\text{bonds}} + V_{\text{angles}} + V_{\text{dihedrals}} + V_{\text{impropers}} + V_{\text{crossterms}} + V_{\text{charges}} + V_{\text{vdw}} \quad (1)$$

The first five terms ( $V_{\text{bonds}}$ ,  $V_{\text{angles}}$ ,  $V_{\text{dihedrals}}$ ,  $V_{\text{impropers}}$ , and  $V_{\text{crossterms}}$ ) represent the bonding interactions, and the last two

terms ( $V_{\text{charges}}$  and  $V_{\text{vdw}}$ ) account for the nonbonding interactions between atomic pairs. The van der Waals interactions are calculated with a cutoff distance of 9.5  $\text{\AA}$ , and the van der Waals cross terms are derived from the Waldman and Hagler combining rules.<sup>80</sup> The electrostatic interactions are computed using the Ewald summation.<sup>81</sup>

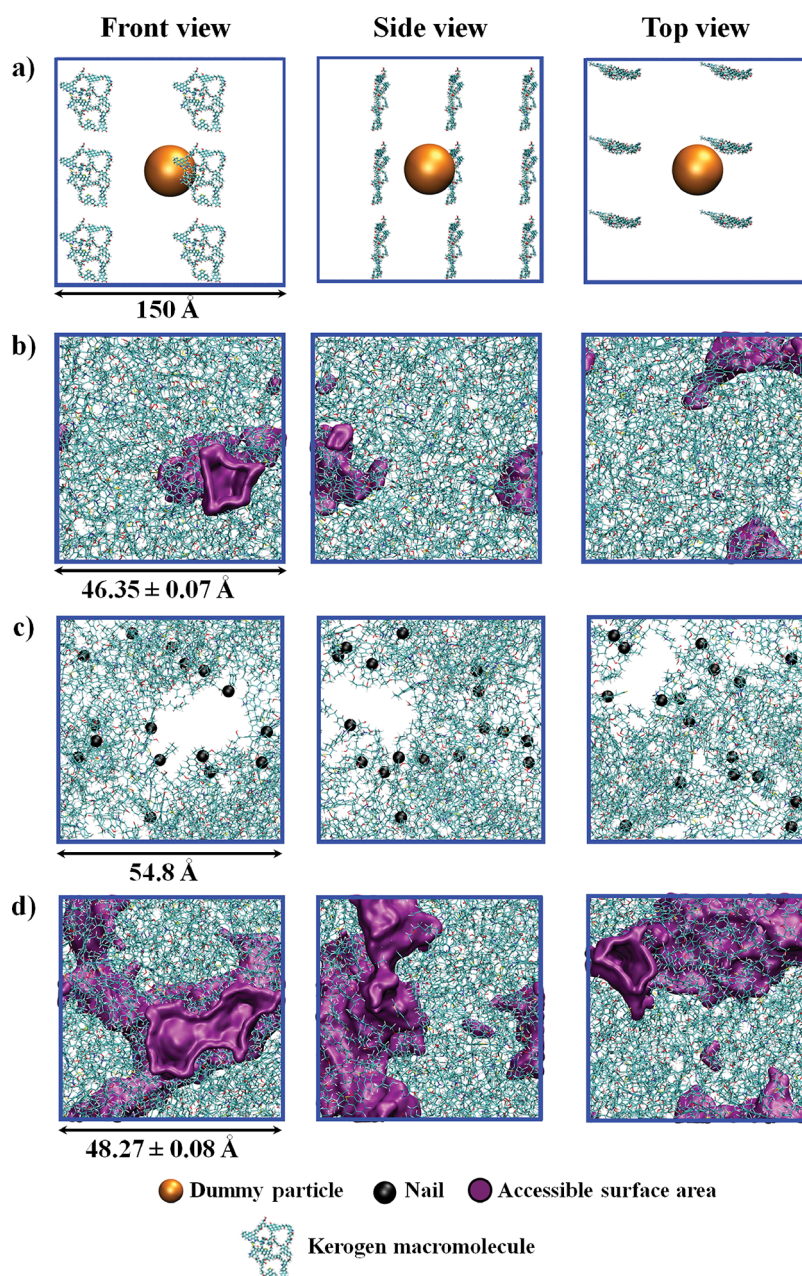
Molecular dynamics (MD) simulations are performed in the canonical (NVT) and isothermal–isobaric (NPT) ensemble in order to create kerogen matrix. The NPT ensemble is used to investigate adsorption and swelling of the kerogen matrix. MD simulations are applied by using the large-scale atomic molecular massively parallel simulator (LAMMPS) software<sup>82</sup> (stable version 31<sup>st</sup> March 2017). The time steps are, respectively, 1.0 and 0.1 fs in MD simulations in the NVT and NPT ensembles. The periodic boundary conditions (PBC) are applied in the three directions of space. The temperature and the pressure are, respectively, controlled by the Nosé–Hoover thermostat<sup>83,84</sup> and barostat<sup>85,86</sup> with a relaxation time of 1 ps.

The hybrid MD-GCMC method<sup>87</sup> implemented in LAMMPS is used to investigate adsorption of  $CO_2$  and hydrocarbons and the swelling of the kerogen matrix. The MD-GCMC method is performed as follows: a GCMC cycle including 2500 GCMC exchanges (addition and deletion are each attempted with 50% probability) and 2500 GCMC moves (translation and rotation are each attempted with 50% probability) are performed after every 10 000 MD steps. In GCMC simulations, pressure and fugacity coefficient are required as input. As in our previous work,<sup>62</sup> we calculated the fugacity coefficient using the Thermosolver software<sup>88,89</sup> (GCMC simulations are performed to verify that the experimental density of each substance studied agrees with the one predicted by the force field. The results are presented in Table S2). After each GCMC simulation, the number of atoms changes in the simulation box, therefore the number of atoms is updated before each MD simulations. The MD simulations are carried in the NPT ensemble using the same time step, thermostat and barostat as stated above. They allow kerogen and gas molecules to relax. Therefore, the system is free to shrink or swell during the MD simulations. The hybrid simulation characteristics are listed in Table S3 in the SI.

**Characterization Methods.** We use the same methods in this work as in Tesson and Firoozabadi<sup>62</sup> to calculate the porosity, accessible surface area ( $S_{\text{acc}}$ ), and pore size distribution (PSD). In the following, a summary is presented.

- The porosity is computed by the Herrera et al.<sup>65</sup> method. The principle consists of inserting probe molecules randomly inside the simulation box. If the inset probe molecule does not overlap with the kerogen atoms, then the insertion is accepted, otherwise it is rejected.
- The accessible surface area is calculated by the Düren et al.<sup>90</sup> method. The principle consists of rolling the probe molecule on the surface of the pores of the kerogen matrix.
- The pore size distribution is obtained by the Bhattacharya and Gubbins<sup>91</sup> method. The principle is based on inserting particles randomly in the simulation box, increasing their size, and determining the largest sphere from the center of mass of probe molecule to the surface of the pores.
- The volumetric strain is defined as follows:





**Figure 2.** Front, side, and top view of the simulation box at different stages of the molecular dynamics relaxation procedure. (a) Initial orthorhombic simulation box of dimensions  $150 \times 150 \times 150 \text{ \AA}^3$ . (b) Accessible surface area of the final simulation box without nails at  $T = 298.15 \text{ K}$  and  $P = 1 \text{ atm}$ . (c) Initial simulation box of stage 9 of the MD relaxation procedure in which the 17 nailed atoms are highlighted in black. (d) Accessible surface area of the final simulation box with nails:  $T = 298.15 \text{ K}$  and  $P = 1 \text{ atm}$ .

$$Q_v = \frac{V_{\text{box with kerogen and adsorbate}} - V_{\text{box with kerogen and w/o adsorbate}}}{V_{\text{box with kerogen and w/o adsorbate}}} \quad (2)$$

where  $V_{\text{box with kerogen and adsorbate}}$  and  $V_{\text{box with kerogen and w/o adsorbate}}$  are, respectively, the volume of the swollen and initial simulation box.

The porosity and accessible surface area are calculated by helium ( $\sigma_{\text{He}} = 2.9 \text{ \AA}$ ) and nitrogen (simplified by a single sphere with  $\sigma_{\text{N}_2} = 3.653 \text{ \AA}$ ) probe molecules, respectively. The nitrogen molecule is simplified by a single sphere.

## ■ KEROGEN MATRIX

**Creation.** Kerogen matrix is created using the graphical user interface (GUI) of the Medea software.<sup>71</sup> The force field

parameters are applied and the kerogen molecules are relaxed by “simple force field minimization” and “simple force field dynamics” of Medea modules. Seventeen kerogen macromolecules and one dummy particle ( $\sigma_{\text{DP}} = 33 \text{ \AA}$ ) are placed inside an orthorhombic cell of dimensions  $150 \times 150 \times 150 \text{ \AA}^3$  (initial cell density is  $0.03 \text{ g cm}^{-3}$ ). The initial configuration is shown in Figure 2a. Our MD relaxation procedure is applied; the process is summarized in Table 1. In contrast to our previous work,<sup>62</sup> we add a refinement stage (stage 9) in which the dummy particle is removed and a simulation of 100 ns in the NPT ensemble is performed in order to relax the system. We find that the pore system collapses. At the beginning of stage 9, the porosity is  $\sim 30\%$ , after 100 ns, it reduces to  $1.7 \pm 0.1\%$ . The accessible surface area after the pore collapse is



**Table 1. Molecular Dynamics Relaxation Procedure to Create the Flexible Kerogen Matrix<sup>a</sup>**

stage	ensemble	temperature (K)	pressure (atm)	time (ns)
1	NVT	298.15		1
2	NVT	298.15 → 1000		1
3	NVT	1000		1
4	NPT	1000 → 700	100	1
5	NPT	700 → 500	100	1
6	NPT	500 → 298.15	100	1
7	NPT	298.15	100 → 1	1
8	NPT	298.15	1	10
9	NPT	298.15	1	100

<sup>a</sup>Before starting stage 9, the dummy particle is removed and the nails are placed in the periphery of the large pores.

shown in Figure 2b (also listed in Table 2). The structure characteristics are provided in Table 2 and the PSD is presented in Figure S1. The pores are small and cannot host propane, *n*-butane, *i*-butane, and *n*-pentane. To prevent the pore collapse and to create a kerogen matrix with a high porosity (over 10%) we examine three different processes. In two of the methods in addition to kerogen molecules we place, at the beginning of stage 1, inside the simulation box: (i) 12 asphaltene/resin molecules from Collell et al.,<sup>64</sup> in the other (ii) 21 immature asphaltene molecules from León-Barreneche et al.<sup>92</sup> The asphaltene/resin and asphaltene molecules are used to fill the small pores to keep the large pores intact at the end of the MD relaxation process. The pore system collapses in these two methods.

In the third approach, at the beginning of stage 9, we nail a limited number of atoms. The nails are located at the periphery of the pores. The position and the number of the nails are selected to provide a porosity of about 10%. A small number of nails is used to keep the structure flexible. Carbon atoms located at the center of different polyaromatic clusters in kerogen macromolecules are used as nail centers. The nailed atoms (located at the rigid part of the molecule) will act as a ball joint and the polyaromatic cluster as a barrier preventing the shrinkage of the pore. In this work, at the beginning of stage 9, we examine different number of nails. Among different number of nails we select 17 nails. All the 17 kerogen macromolecules have at least one part in contact with the largest pore. However, only 15 kerogen macromolecules have polyaromatic clusters located at the periphery of the largest pore (13 kerogen macromolecules have one nailed atom and 2 have two nailed atoms). During the simulation, the nailed atoms are not included in the time integration to hold these atoms stationary. The nailed atoms are depicted in Figures 2c and S2. The nailing allows the high porosity from the pressure increase to be kept; the system does not collapse. The accessible surface area (after implementation of nailing) is shown in Figure 2d and the structure characteristics are

provided in Table 2 (they are also reported as a function of the number of nails in Table S4).

**Reversibility of Structural Properties and *n*-Pentane Swelling.** First, we analyze the microstructure of the nailed kerogen matrix at 298.15 K to a pressure of 200 atm without adsorbate to investigate the effect of pressure on structure integrity. MD simulations are performed in the NPT ensemble for 10 ns. We find that the porosity, accessible surface area, and pore size distribution (Figure S1 and Table S5) are not significantly affected by the pressure increase. The box size and skeletal density increase with pressure increase, whereas the porosity and accessible surface area decrease with pressure increase. The structural changes of the kerogen matrix are reversible in the nailed kerogen matrix.

Then, we examine *n*-pentane swelling in the nailed kerogen matrix at 298.15 K and 1 atm to verify the model. The structural properties are presented in Table 3, and the pore size distribution and *n*-pentane accessible surface area are, respectively, presented in panels 3a, 3b, and 3c of Figure 3. The results show that the lattice, porosity, and accessible surface area increase, respectively, from  $48.27 \pm 0.08 \text{ \AA}$ ,  $10.8 \pm 0.2\%$ , and  $360 \pm 11 \text{ m}^2 \text{ g}^{-1}$  to  $49.9 \pm 0.3 \text{ \AA}$ ,  $16.0 \pm 0.6\%$ , and  $698 \pm 21 \text{ m}^2 \text{ g}^{-1}$ . The resulting volumetric strain is about 9%. The calculated volumetric strain is lower than the experimental data<sup>28,30–32</sup> which is between 15 and 24%. The 9% increase from our simulations show that the nailed kerogen can describe the swelling. There is a shift in the pore size distribution to larger pores from the introduction of *n*-pentane to kerogen matrix (Figure 3a). By analyzing the trajectory, we find that the matrix deforms and paths are created allowing the *n*-pentane molecules to go back and forth from one pore to another (Figures 3b and c).

## RESULTS AND DISCUSSION

**Adsorption and Kerogen Swelling.** We analyze gas adsorption isotherms in flexible kerogen matrix at  $T = 393.15 \text{ K}$  to a pressure of 400 atm by carbon dioxide, methane, ethane, and propane, and to a pressure of 20 atm for *n*-butane and *i*-butane. The adsorption isotherms are calculated following a sequential method, i.e., the starting configuration of each pressure is the final configuration of the previous one. For each thermodynamic point and for all systems we have verified that the equilibrium is reached by examining temperature, pressure and loading (results for *n*-butane at 20 atm are presented in Figure S4). The density of each system is presented in Table S6. (Note that the density increase from CO<sub>2</sub> adsorption and dissolution in kerogen matrix is more than hydrocarbons including *n*-C<sub>3</sub>H<sub>12</sub>. The increase from CO<sub>2</sub> dissolution is in line with density increase of hydrocarbon liquids from dissolution of CO<sub>2</sub>.<sup>93</sup>) The adsorption affects swelling in a flexible kerogen matrix. We also have verified the effect of the nails on the structural properties by a direct method. The CH<sub>4</sub> and CO<sub>2</sub> adsorption isotherms at  $T = 393.15 \text{ K}$  and  $P = 400 \text{ atm}$  are calculated based on the starting configuration from the

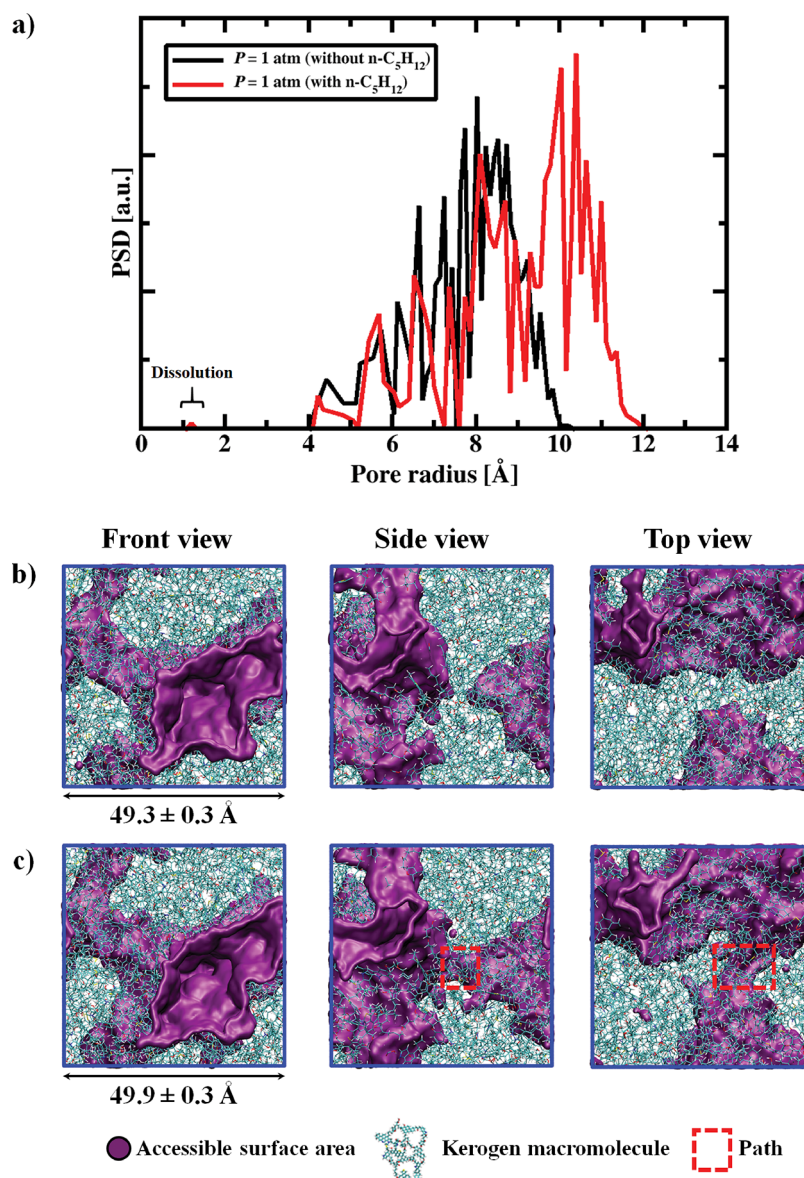
**Table 2. Structure Characterization of the Kerogen Matrix at the End of the MD Relaxation Procedure ( $T = 298.15 \text{ K}$  and  $P = 1 \text{ atm}$ ) without and with 17 Nails<sup>a</sup>**

system	lattice (Å)	box density (g cm <sup>-3</sup> )	skeletal density (g cm <sup>-3</sup> )	porosity (%)	accessible surface area (m <sup>2</sup> g <sup>-1</sup> )
w/o nail	$46.35 \pm 0.07$	$1.102 \pm 0.005$	$1.121 \pm 0.004$	$1.7 \pm 0.1$	$103 \pm 8$
with nails	$48.27 \pm 0.08$	$0.976 \pm 0.005$	$1.055 \pm 0.004$	$10.8 \pm 0.2$	$360 \pm 11$

<sup>a</sup>The skeletal density is based on the volume measured excluding the pores and the void spaces between particles.

**Table 3.** Structure Characterization of the Nailed Kerogen Matrix from Saturation by Liquid *n*-Pentane at  $T = 298.15$  K and  $P = 1$  atm

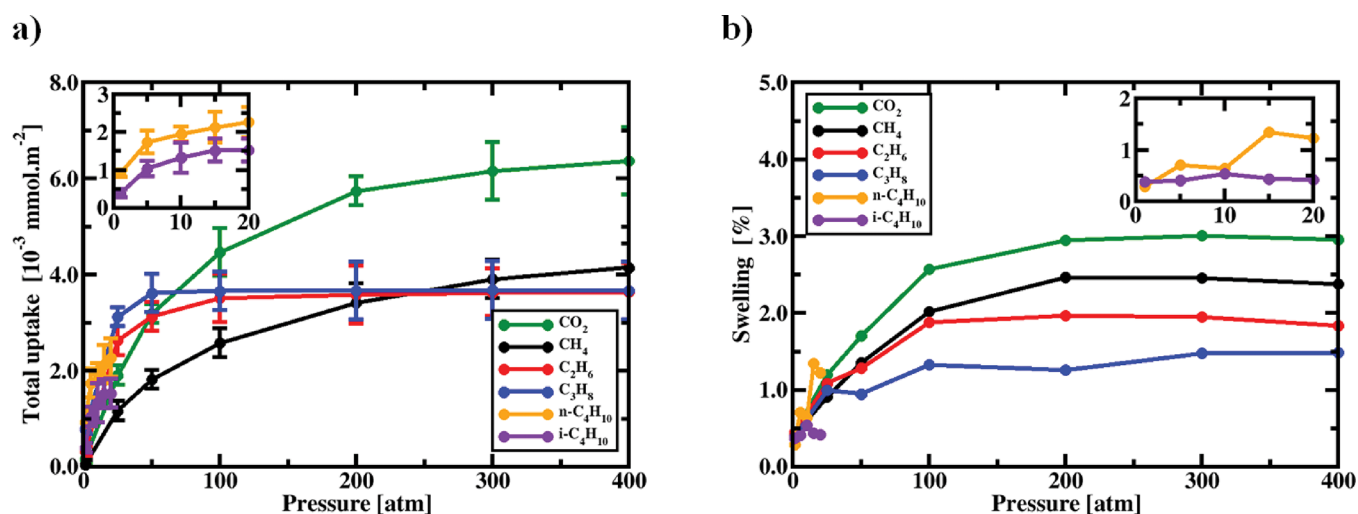
lattice (Å)	porosity (%)	accessible surface area ( $\text{m}^2 \text{g}^{-1}$ )	total uptake ( $\times 10^{-3} \text{ mmol m}^{-2}$ )	$Q_v$ (%)
$49.9 \pm 0.3$	$16.0 \pm 0.6$	$698 \pm 21$	2.49	9

**Figure 3.** Pore size distribution and views from front, side, and top of the nailed simulation box after *n*-pentane saturation. (a) Pore size distribution before (black line) and after (red line) *n*-pentane saturation. Accessible surface area (b) before saturation by *n*-pentane, and (c) after saturation by *n*-pentane (in the nailed kerogen):  $T = 298.15$  K and  $P = 1$  atm.

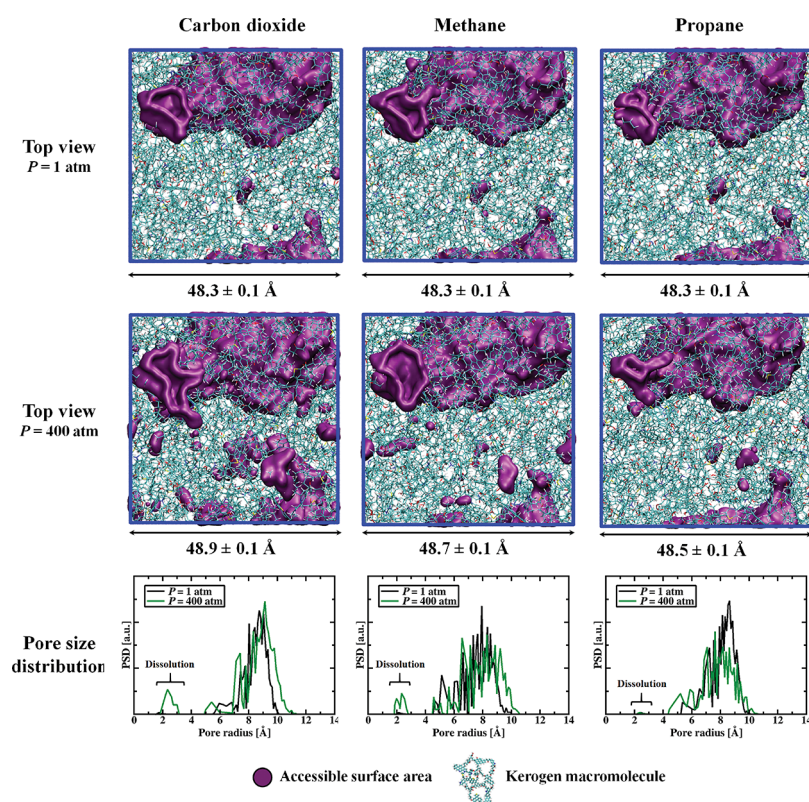
final configuration of the MD relaxation procedure. The properties calculated by the direct and sequential methods are close. They are presented in Table S7.

Figure 4a shows that the total uptake reaches a plateau, of  $3.58 \times 10^{-3} \text{ mmol m}^{-2}$  by ethane at  $\sim 200$  atm;  $3.66 \times 10^{-3} \text{ mmol m}^{-2}$  by propane at  $\sim 100$  atm;  $2.13 \times 10^{-3} \text{ mmol m}^{-2}$  by *n*-butane at  $\sim 15$  atm and  $1.52 \times 10^{-3} \text{ mmol m}^{-2}$  by *i*-butane at  $\sim 15$  atm. The temperature is 393.15 K. The total uptake of carbon dioxide ( $6.37 \times 10^{-3} \text{ mmol m}^{-2}$  at 400 atm) and methane ( $4.15 \times 10^{-3} \text{ mmol m}^{-2}$  at 400 atm) have increasing trend between 1 and 400 atm. The trends are consistent with absolute adsorption results based on measurement of excess adsorptions.<sup>25,26,94</sup> The trends are also consistent with

molecular simulation results by Collell et al.<sup>55</sup> (methane and ethane), Sui et al.<sup>7</sup> (methane and carbon dioxide), Vasileiadis et al.<sup>52</sup> (methane, ethane, *n*-butane, and carbon dioxide) in rigid kerogen matrices. Ho et al.<sup>49</sup> (methane, carbon dioxide, and helium), Tesson and Firoozabadi<sup>62</sup> (methane), and Wu and Firoozabadi<sup>70</sup> (methane) show also the same trends in flexible kerogen matrices. The total uptake of  $\text{CO}_2$  is  $\sim 1.7$  times higher (in mol) than the total uptake of  $\text{CH}_4$  at 393.15 K and 200 atm. The result has the same trend as found by Ho et al.<sup>49</sup> in type II-D kerogen matrix (the total uptake of  $\text{CO}_2$  is  $\sim 1.6$  times higher than the total uptake of  $\text{CH}_4$  at 300 K and 192 atm). Figure 4a indicates that the *n*-butane adsorption is about  $\sim 1.5$  times higher than the *i*-butane adsorption at 393.15



**Figure 4.** (a) Total uptake and (b) swelling vs pressure at  $T = 393.15$  K in carbon dioxide (green), methane (black), ethane (red), propane (blue), *n*-butane (orange), and *i*-butane (purple) in the flexible nailed kerogen matrices.



**Figure 5.** Top view of the accessible surface area and pore size distribution at  $T = 393.15$  K and  $P = 1$  and 400 atm in carbon dioxide, methane and propane. Note higher dissolution of  $\text{CO}_2$  in kerogen matrix than methane, and less by propane at 400 atm.

K and 20 atm. This difference may be due to molecular volumes ( $45 \pm 2 \text{ \AA}^3$  for *n*-butane<sup>95</sup> and  $58 \pm 2 \text{ \AA}^3$  for *i*-butane<sup>95</sup>) and molecular areas ( $20.5 \pm 0.4 \text{ \AA}^2$  for *n*-butane<sup>95</sup> and  $21.9 \pm 0.7 \text{ \AA}^2$  for *i*-butane<sup>95</sup>). The same large difference is also reported in measurements using immature kerogen samples.<sup>24–26</sup>

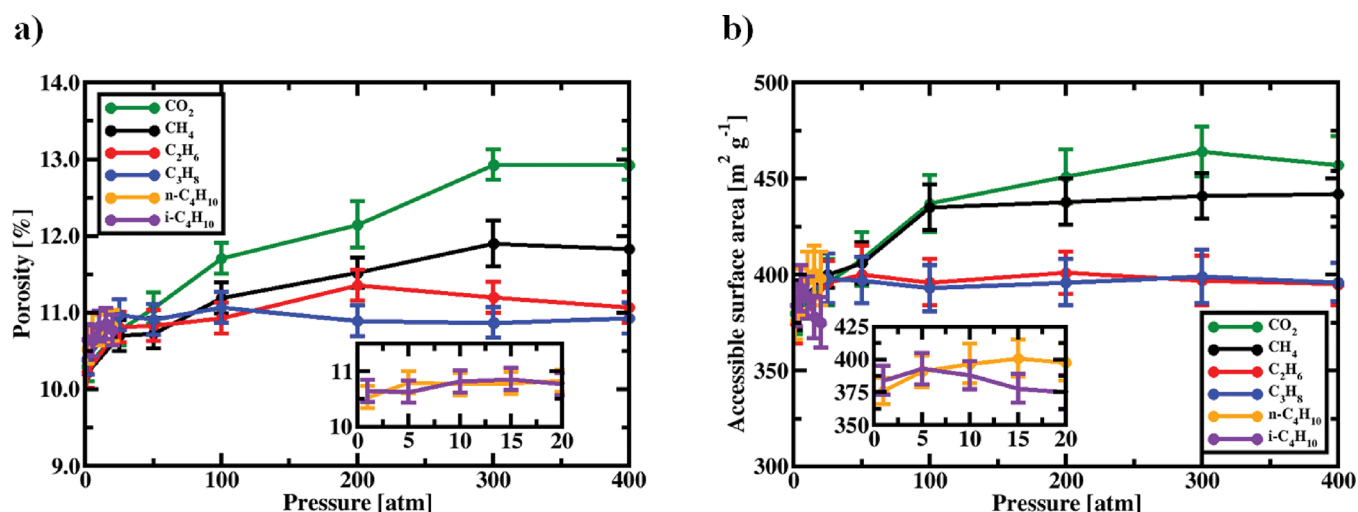
Figure 4b shows that kerogen matrix swells more in adsorbates by smaller molecules ( $\text{CO}_2 > \text{CH}_4 > \text{C}_2\text{H}_6 > \text{C}_3\text{H}_8$  at 393.15 K and 400 atm and  $n\text{-C}_4\text{H}_{10} > i\text{-C}_4\text{H}_{10}$  at 393.15 K and 20 atm). The flexibility of the kerogen matrix allows the kerogen microstructure to deform and to create paths. Small molecules can dissolve in the kerogen matrix. Pore

size distribution in Figure 5 and the highlighted dissolved molecules in Figures S3 give strong evidence of dissolution (see the pore size distribution from adsorption of  $\text{CO}_2$  and  $\text{CH}_4$  in Figure 5) and creation of small pores by adsorption. These results demonstrate the need for considering kerogen flexibility in kerogen swelling and adsorption simulations.<sup>24–26</sup>

**Structural Characterization.** We have analyzed kerogen porosity and accessible surface area in flexible kerogen matrix at  $T = 393.15$  K to a pressure of 400 atm in  $\text{CO}_2$ ,  $\text{CH}_4$ ,  $\text{C}_2\text{H}_6$ , and  $\text{C}_3\text{H}_8$  and to a pressure of 20 atm in  $n\text{-C}_4\text{H}_{10}$  and  $i\text{-C}_4\text{H}_{10}$ .

The initial kerogen structure porosity and accessible surface area are, respectively,  $10.8 \pm 0.2\%$  and  $360 \pm 11 \text{ m}^2 \text{ g}^{-1}$  (Table





**Figure 6.** a) Porosity, and b) accessible surface area vs pressure at  $T = 393.15$  K in carbon dioxide (green), methane (black), ethane (red), propane (blue),  $n$ -butane (orange), and  $i$ -butane (purple) in the swollen nailed kerogen matrix.

2). Figure 6a shows that upon gas adsorption, in the flexible kerogen structure, the porosity increases to  $12.9 \pm 0.2\%$  by  $\text{CO}_2$ ,  $11.8 \pm 0.3\%$  by  $\text{CH}_4$ ,  $11.1 \pm 0.2\%$  by  $\text{C}_2\text{H}_6$ , and  $10.9 \pm 0.2\%$  by  $\text{C}_3\text{H}_8$  at 400 atm. Whereas, in  $n$ -butane ( $10.8 \pm 0.2\%$ ) and  $i$ -butane ( $10.8 \pm 0.2\%$ ), the porosity fluctuates around the initial value from 1 to 20 atm. Figure 6b shows that from gas adsorption, the accessible surface area increases to  $457 \pm 15 \text{ m}^2 \text{ g}^{-1}$  by  $\text{CO}_2$ ,  $442 \pm 12 \text{ m}^2 \text{ g}^{-1}$  by  $\text{CH}_4$ ,  $395 \pm 11 \text{ m}^2 \text{ g}^{-1}$  by  $\text{C}_2\text{H}_6$  and  $396 \pm 10 \text{ m}^2 \text{ g}^{-1}$  by  $\text{C}_3\text{H}_8$  at 400 atm and to  $398 \pm 14 \text{ m}^2 \text{ g}^{-1}$  by  $n$ - $\text{C}_4\text{H}_{10}$  and  $375 \pm 13 \text{ m}^2 \text{ g}^{-1}$  by  $i$ - $\text{C}_4\text{H}_{10}$  at 20 atm. With increasing pressure, kerogen microstructure changes, the accessible surface area increases and the kerogen swelling may generate larger pores (Figures 6a, b, S5, and S6). These results are in agreement with Ho et al.<sup>49</sup> in type II-D flexible kerogen matrix. In contrast to the work by Ho et al.<sup>49</sup> we find that small gas molecules can dissolve in the solid increasing the swelling of the kerogen matrix. Note the sudden change in the slope of the accessible surface area from 50 to 100 atm (Figure 6b). This is due to the fact that small gas molecules dissolve in the solid and create small pores. These results are in line with the pore size distribution (Figures 5 and S5). The increase in pressure results in swelling which allows gas to access spaces that it cannot at lower pressure. The kerogen molecular flexibility has a significant effect on adsorption and kerogen swelling.

## CONCLUSIONS

In this work we have proposed a new method to create and engineer the kerogen porosity based on flexible kerogen macromolecules using a dummy particle and a limited number of nails to prevent the collapse of the pore structure of the kerogen. We use the type II-A kerogen macromolecules. Without the nails, the system would collapse and the porosity would decrease drastically. By using a dummy particle we create large enough pores to accommodate adsorption of methane, ethane, propane,  $n$ -butane,  $i$ -butane, carbon dioxide, and saturation by  $n$ -pentane. The method can be used with other types of kerogen molecules. The adsorption of  $\text{CH}_4$ ,  $\text{C}_2\text{H}_6$ ,  $\text{C}_3\text{H}_8$ , and  $\text{CO}_2$  (393.15 K to a pressure of 400 atm),  $n$ - $\text{C}_4\text{H}_{10}$  and  $i$ - $\text{C}_4\text{H}_{10}$  (393.15 K to a pressure of 20 atm) and saturation by liquid  $n$ - $\text{C}_5\text{H}_{12}$  (298.15 K and 1 atm) are predicted using the hybrid Molecular Dynamics-Grand

Canonical Monte Carlo (MD-GCMC) method. The kerogen swelling is also investigated by MD-GCMC simulations. The key element of creating a kerogen matrix is the use of a limited number of nails to avoid porosity collapse. The use of the nail technique can be further refined to achieve full swelling in the future. The main findings from our work are

1. The flexibility of kerogen matrix allows the kerogen microstructure to deform and to create paths. Small molecules can dissolve in the kerogen matrix. Ethane and propane adsorption at 393.15 K reaches a plateau at  $\sim 200$  and  $\sim 100$  atm, respectively. Methane and carbon dioxide adsorption shows increasing trend even to 400 atm. Carbon dioxide adsorption is about  $\sim 1.7$  times higher than methane adsorption (mol basis) at 393.15 K and 400 atm.
2. Whereas  $n$ -butane and  $i$ -butane molecules have the same molecular weight and close bulk gas densities,  $n$ -butane adsorption is about  $\sim 1.5$  times higher than  $i$ -butane adsorption at 393.15 K and 20 atm.
3. Adsorption leads to structural change in the flexible kerogen matrix; the swelling of the kerogen with gases decreases with increasing the size of the molecules ( $\text{CO}_2 > \text{CH}_4 > \text{C}_2\text{H}_6 > \text{C}_3\text{H}_8$  at 393.15 K and 400 atm). The swelling has a monotonic increase with increase in pressure and may reach a plateau. It does not show a nonmonotonic trend with pressure as some literature suggests.
4. The process of swelling in the hydrocarbon liquid  $n$ - $\text{C}_5\text{H}_{12}$  is different than that in hydrocarbon gases. The pore structure changes and porosity increases more significantly by the light hydrocarbon liquid  $n$ - $\text{C}_5\text{H}_{12}$  than in gases.

In the future, we plan to further investigate the isothermal adsorptions of several hydrocarbons (from  $\text{CH}_4$  to  $\text{C}_{14}\text{H}_{30}$  using MD-GCMC and configurational bias-GCMC methods) and the system size effect by increasing the number of kerogen macromolecules and/or the number of dummy particles. Results will be published as they become available.

## ■ ASSOCIATED CONTENT

## ● Supporting Information

The Supporting Information is available free of charge on the ACS Publications website at DOI: 10.1021/acs.jpcc.9b04592.

Composition and structural parameters of type II-A kerogen macromolecule, bulk density, hybrid simulations characteristics, structure characterization of the kerogen matrix based on the MD relaxation procedure without and with nails, structure characterization of the kerogen matrix at different pressures, box density, structure characterization of the kerogen matrix using the sequential and direct isotherm calculation approaches, pore size distribution of the kerogen matrix without and with nails at  $T = 298.15$  K, front view of the simulation box and zoom on one nailed atom, top view of the simulation box with  $\text{CO}_2$  and hydrocarbons (methane and propane) dissolved in an isolated micropore, average temperature, pressure, and number of  $n$ -butane molecules in the simulation box at 393.15 K and 20 atm, pore size distribution at three different pressures and  $T = 393.15$  K, and views of the accessible surface area at  $P = 400$  atm and  $T = 393.15$  K (PDF)

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## Notes

The authors declare no competing financial interest.

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